

# X-ray structural studies of nitrogen diffusion in Dy<sub>2</sub>Fe<sub>17</sub>

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The reaction between N<sub>2</sub> and Dy<sub>2</sub>Fe<sub>17</sub> has been studied by thermopiezic analysis on 20–25 μm sized powders in the temperature range 400–500 °C. Partially nitrated powders were analyzed using CuK<sub>α</sub> x-ray diffraction and thermomagnetic techniques. Both high angle x-ray and thermomagnetic data show only the presence of Dy<sub>2</sub>Fe<sub>17</sub> and Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3-δ</sub> (δ<0.3) with no evidence of intermediate compositions. The results of the x-ray diffraction experiments at several Bragg peaks were simulated using a two phase model structure: a Dy<sub>2</sub>Fe<sub>17</sub> core with a Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> surface layer. The results show that at low temperatures the nitride layer is too thin to account for all of the nitrogen absorbed by the sample, indicating that a significant amount of the nitrogen diffused into the core of the particles, presumably along grain boundaries.

During a gas–solid reaction, nitrogen diffuses into R<sub>2</sub>Fe<sub>17</sub> (R=rare earth), occupying interstitial sites and expanding the lattice without changing the crystal structure. The enhancement of the magnetic properties was observed<sup>1</sup> as a result of interstitial nitrogen diffusion in R<sub>2</sub>Fe<sub>17</sub>. Neutron powder diffraction<sup>2</sup> showed that the R<sub>2</sub>Fe<sub>17</sub> and R<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> phases are in equilibrium during the reaction. However, it was observed<sup>3,4</sup> that a continuous solid solution R<sub>2</sub>Fe<sub>17</sub>N<sub>x</sub> (0<x<3) is formed on annealing partially nitrated powders. In this study we use x-ray diffraction and thermomagnetic techniques to characterize nitrogen diffusion in the 2-17 structure. Nitrogen diffusion in the 2-17 structure typically occurs above 350 °C, and significant diffusion through extended defects such as grain boundaries at 400 °C has been observed using metallography.<sup>5</sup>

The polycrystalline Dy<sub>2</sub>Fe<sub>17</sub> alloy was prepared by induction melting of appropriate amounts of Dy and Fe, followed by vacuum annealing at 1173 K for two weeks. Induction melting ensures homogeneity of alloys and mass loss was below 0.03% during preparation. The homogenized ingot was ground and sieved to select powder sizes between 20 and 25 μm. The powder size was confirmed by scanning electron microscopy. Nitrogen diffusion was performed in a thermopiezic analyzer (TPA) at a starting pressure of 1 bar and temperatures ranging from 400 °C (590 min) to 500 °C (25 min) to obtain Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub>. The amount of nitrogen diffused into the sample was obtained directly from the gas pressure change in the TPA. Structural analyses on Dy<sub>2</sub>Fe<sub>17</sub>, before and after the gas–solid reaction, were carried out using CuK<sub>α</sub> radiation on an automated Nicolet–Stöe powder diffractometer with a graphite monochromator in the diffracted beam. Thermomagnetic analyses were done using a Perkin–Elmer thermogravimetric analyzer (TGA) in a small field gradient.

The x-ray diffraction pattern of Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub> is shown in Fig. 1. As a consequence of nitrating, a new phase was formed with the same structure as Dy<sub>2</sub>Fe<sub>17</sub> but with the Bragg peaks shifted towards lower angles indicating an expansion of the unit cell. This shift is shown more clearly in

Fig. 2, where the (300) peaks of Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub> (top) are compared with those (bottom) of pure Dy<sub>2</sub>Fe<sub>17</sub> (N<sub>0</sub>) and Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> (N<sub>3</sub>). Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub> clearly contains both Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> and unreacted Dy<sub>2</sub>Fe<sub>17</sub>. The position of the Dy<sub>2</sub>Fe<sub>17</sub> peak is shifted towards lower angles, due to the expansion of the unreacted core, while that of Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> is shifted slightly towards higher angles. Careful examination of the (332) Dy<sub>2</sub>Fe<sub>17</sub> and Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> diffraction peaks (inset of Fig. 1), which are well separated, shows no evidence of the existence of an intermediate composition phase. Using TGA two distinct Curie temperatures, T<sub>c1</sub>=128 °C and T<sub>c2</sub>=445 °C are detected as shown in Fig. 3. T<sub>c1</sub> is 28 °C higher than the Curie temperature of Dy<sub>2</sub>Fe<sub>17</sub> and T<sub>c2</sub> is 5 °C lower than the Curie temperature of Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>. The x-ray and the TGA data are thus in agreement, as T<sub>c</sub> changes with the lattice expansion of Dy<sub>2</sub>Fe<sub>17</sub>. Even if the observed experimental data only show the existence of Dy<sub>2</sub>Fe<sub>17</sub> and Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>, they are not at equilibrium at 500 °C. After subsequent annealing for 60 h at 480 °C, a uniform Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub> solid solution was obtained. Further work is in progress to study this equilibrium phase. Because Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> and Dy<sub>2</sub>Fe<sub>17</sub> are not in equilibrium, we tried to estimate the amount of the undetected intermediate phase (in the interface between Dy<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> and Dy<sub>2</sub>Fe<sub>17</sub>) by comparing the x-ray patterns of crushed Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub>, shown in Fig. 2(b), with

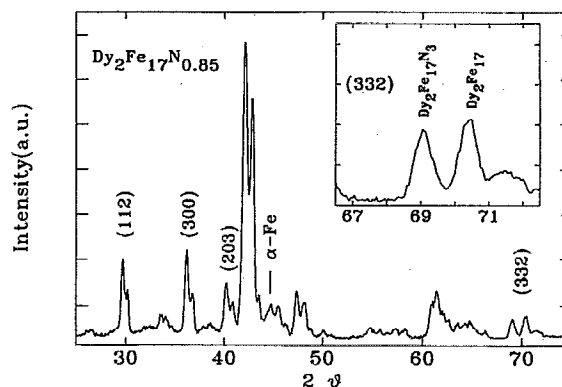


FIG. 1. The x-ray diffraction pattern of Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub> for nitrogen diffused at 500 °C for approximately 25 min. Inset: (332) peak of Dy<sub>2</sub>Fe<sub>17</sub>N<sub>0.85</sub>.

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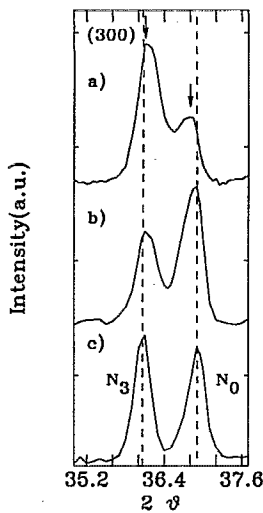


FIG. 2. (a) The (300) diffraction peak of  $\text{Dy}_2\text{Fe}_{17}\text{N}_{0.85}$  (powder sizes between 20 and 25  $\mu\text{m}$ ). (b) The diffraction peak of the subsequently crushed  $\text{Dy}_2\text{Fe}_{17}\text{N}_{0.85}$ . (c) The (300) peak of a mixture of pure  $\text{Dy}_2\text{Fe}_{17}$  and  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  powders in the ratio 1:1.

those (bottom of Fig. 2) of pure  $\text{Dy}_2\text{Fe}_{17}$  ( $\text{N}_0$ ) and  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  ( $\text{N}_3$ ). Note that for the crushed  $\text{Dy}_2\text{Fe}_{17}\text{N}_{0.85}$  powder the x-ray peaks are mostly relaxed to the unshifted positions. Fitting shows that the possible amount of the intermediate phase is much lower than the amount of the  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  phase.

Nitrogen distribution can be estimated from the ratio of the intensities of the diffraction peaks by using a simple model where the core is nitrogen-free and the surface layer is fully nitrated as shown schematically in Fig. 4. Estimating the volume fractions is complicated because the  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  phase coats the  $\text{Dy}_2\text{Fe}_{17}$  phase and so attenuates the x-ray scattering. In a multilayered system the intensity of the reflected beam from the  $i$ th layer can be expressed as

$$I_i = I_0 e^{-\sum_{j=1}^{i-1} (2d_j \mu_j / \sin \theta)} \int_0^{d_i} e^{-2x \mu_i / \sin \theta} dx \int dS, \quad (1)$$

where  $I_0$  and  $\theta$  are the intensity and angle of the incident beam,  $d_i$  and  $\mu_i$  are the thickness and absorption coefficient of the  $i$ th layer, respectively, and  $S$  is the surface area illuminated by the beam.

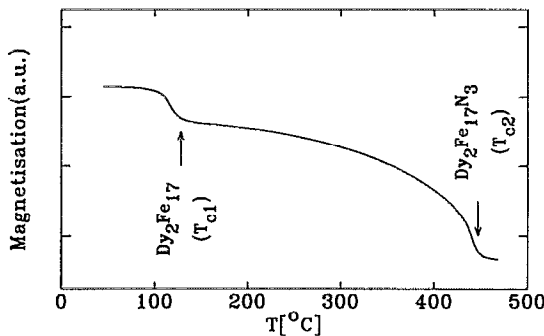


FIG. 3. Thermogravimetric analyses of  $\text{Dy}_2\text{Fe}_{17}\text{N}_{0.85}$ .  $T_{c1}$  correspond to the Curie temperature of the  $\text{Dy}_2\text{Fe}_{17}$  and  $T_{c2}$  to Curie temperature of the  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  phase.

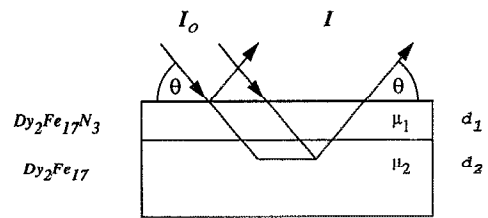


FIG. 4. Two layer model structure used to calculate x-ray diffraction patterns.

nated by the beam. The term  $e^{-\sum_{j=1}^{i-1} (2d_j \mu_j / \sin \theta)}$  comes from the attenuation of the x-ray beam from the top ( $i-1$ ) layers. For the two layer model, the intensity ratio becomes

$$I_1 / I_2 = (\mu_2 / \mu_1) (e^{2d_1 \mu_1 / \sin \theta} - 1), \quad (2)$$

where we have neglected the term  $e^{-2d_2 \mu_2 / \sin \theta}$  as  $d_2 \approx 20 \mu\text{m}$  and  $\mu_2 = 1.577 \mu\text{m}^{-1}$ .

The relative intensities ( $I_1, I_2$ ) were estimated by a simultaneous fitting of the measured (112), (300), and (203) Bragg peaks to Eq. (1) where each Bragg peak is a combination of two Gaussians with position  $p_i$  and width  $w_i$  ( $i = 1, 2$ ), representing the contributions from  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  and  $\text{Dy}_2\text{Fe}_{17}$ . The widths,  $w_1$  and  $w_2$ , are adjusted during the fitting. We note that this model assumes that the nitrogen diffuses uniformly through the bulk of the material. Figure 5 shows the  $\text{CuK}\alpha$  x-ray diffraction patterns of  $\text{Dy}_2\text{Fe}_{17}\text{N}_{0.85}$  samples nitrated at 500  $^\circ\text{C}$ . The solid lines in Fig. 5 are the fits to the experimental data and the dotted lines are the contributions of  $\text{Dy}_2\text{Fe}_{17}$  and  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  calculated from the model. Assuming that the average particle has a rectangular shape with the dimensions  $20 \times 15 \times 10 \mu\text{m}^3$  (this particle shape is an approximate representation deduced from scanning electron microscope photographs) we obtain, using the calculated thicknesses of the layers, that for nitrogen diffusion at 500  $^\circ\text{C}$  approximately 90% of the nitrogen can be accounted for by the intensity of the fully nitrated peak. This shows that almost the entire amount of nitrogen is in the surface layer (the penetration of the  $\text{CuK}\alpha$  in  $\text{Dy}_2\text{Fe}_{17}$  is restricted to approximately 1–2  $\mu\text{m}$ ). To observe the nitrogen

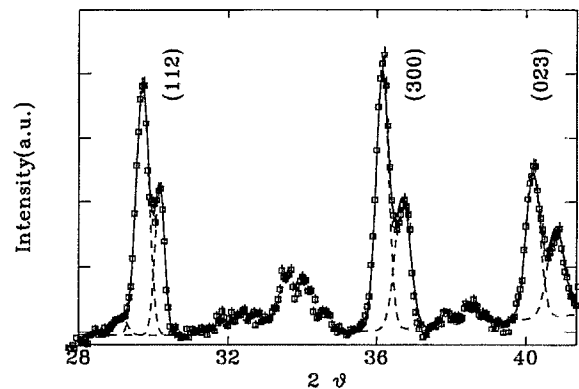


FIG. 5. Simultaneous fitting of (112), (300), and (023) peaks using a two layer model structure. The solid lines are contributions of  $\text{Dy}_2\text{Fe}_{17}$  and  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  calculated from the model.

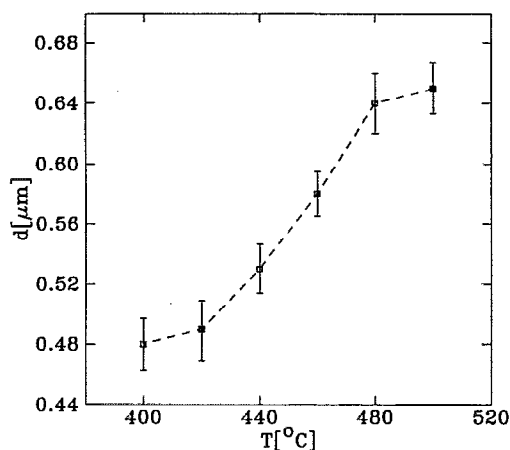


FIG. 6. Effect of reaction temperature on the apparent  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  layer thickness derived from fits to the x-ray diffraction patterns. All samples have the same nominal nitrogen content.

distribution at different temperatures we introduced the same amount of nitrogen (a bulk average of 0.85 atoms per unit formula) to 20–25  $\mu\text{m}$  sized powders at temperatures between 400 and 500  $^\circ\text{C}$ .

The values for the thicknesses of the nitrated layer versus the nitriding temperature is shown in Fig. 6. Despite the fact that all of the nitrated samples have the same nominal composition, the  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  surface layer is clearly thinner in the samples prepared at lower temperatures. In the absence of any evidence for the formation of an intermediate compo-

sition nitride phase, we attribute the apparent nitrogen deficit to the formation of the nitride phase at depths within the particles beyond the penetration range of the  $\text{CuK}\alpha$  radiation ( $\approx 1 \mu\text{m}$ ). For this to happen, the nitrogen must find more rapid diffusion paths than bulk diffusion allows, presumably along extended defects such as grain boundaries. Above 480  $^\circ\text{C}$ , the two layer model accounts for over 90% of the absorbed nitrogen, and we conclude that for these temperatures nitrogen transport is dominated by bulk diffusion.

In conclusion, using x-ray diffraction and a thermomagnetic technique only  $\text{Dy}_2\text{Fe}_{17}$  and  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  phases were observed. The thickness of the nitrogen layer was obtained by fitting x-ray diffraction peaks with a two phase model structure: a  $\text{Dy}_2\text{Fe}_{17}\text{N}_3$  surface layer and a  $\text{Dy}_2\text{Fe}_{17}$  core. Significant nitrogen diffusion through extended defects such as grain boundaries was observed at temperatures below 480  $^\circ\text{C}$ .

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